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**Analog Electronic Circuits**

Prof. Mor M. Peretz

The Center for Power Electronics and Mixed-Signal IC  
 Department of Electrical and Computer Engineering  
 Ben-Gurion University of the Negev, ISRAEL  
 Emails: [morp@bgu.ac.il](mailto:morp@bgu.ac.il)  
 Website: <http://www.ee.bgu.ac.il/~pemic>  
<http://www.ee.bgu.ac.il/~analog>

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**Lesson #4**  
Outline

- Slew-rate (summary)
- Input Impedances
  - Differential
  - Common-Mode
- CMRR
- Effect of feedback on impedances
  - Blackman's theorem
  - Output
    - Current and voltage feedback
  - Input
    - Series and parallel summation
- Instrumentation amplifier
- Stability

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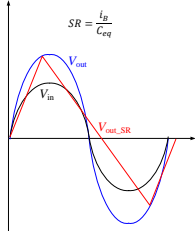
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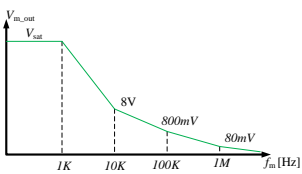

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**Transient response**  
Slew-Rate

$$SR = \frac{I_B}{C_{eq}}$$


Sine wave  $V_{m,out} = \min\left(\frac{SR}{2\pi f_m}, V_{sat}\right)$



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### Input Impedances

$$V_{cm} = \frac{V_1 + V_2}{2}$$

$$V_d = V_1 - V_2$$

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### Input Impedances Differential

$$h_{ie} = \frac{V_r}{I_e} (h_{fe} + 1)$$

$$R_d = 2h_{ie} = 2 \frac{V_r}{I_e} (h_{fe} + 1)$$

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### Input Impedances Common-mode

$$R_e = \frac{1}{h_{oe}}$$

$$R_{cm} = 2R_e (h_{fe} + 1)$$

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### Common-Mode Rejection Ratio (CMRR)

$$CMRR \equiv \frac{A_d}{A_{cm}} = \frac{A_d A_2 A_3}{A_{cm} A_2 A_3}$$

$$V_{cm} = \frac{V_1 + V_2}{2}$$

$$V_d = V_1 - V_2$$

$$V_{out,cm} = A_{cm} V_{cm} = A_{cm} \frac{V_1 + V_2}{2}$$


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### Common-Mode Rejection Ratio (CMRR)

$$V_{out} = A_{cm} V_{cm} + A_d V_d$$

$$\frac{V_{out}}{A_d} = \frac{V_{cm}}{CMRR} + V_d$$

Reflected to input (as done to ALL non-idealities)

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### Blackman's Theorem

$$Z_F = Z_{NF} \frac{1 + \beta A_{SC}}{1 + \beta A_{OC}}$$

Voltage feedback:  $Z_F = \frac{Z_{NF}}{1 + \beta A}$

Current feedback:  $Z_F = Z_{NF} (1 + \beta A)$

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### Effect of feedback Output impedance

Voltage feedback

$$Z_{out\_F} = R_0 \frac{1 + \beta A_{SC}}{1 + \beta A_{OC}}$$

Current feedback

$$Z_{out\_F} = R_0 \frac{1 + \beta A_{SC}}{1 + \beta A_{OC}}$$

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### Effect of feedback Example

R1=10k  
R2=1k  
R0=100

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### Linear regulator Low-Drop Out (LDO)

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### Effect of feedback Input impedance

Series (voltage) summation

$$Z_{In,F} = Z_{NF}(1 + \beta A)$$

Parallel (current) summation

$$Z_{In,F} = \frac{Z_{NF}}{(1 + \beta A)}$$

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### Input Impedances

$$R_{In} = R_2 + \frac{R_1 + r_o}{(1 + \beta A)} \approx R_2$$

$$R_{In,1} = R_2$$

$$R_{In,2} = R_3 + R_4$$

$$R_{In,1,2} = R_2 + R_3$$

$$R_{In} = R_d(1 + \beta A)$$

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### Difference Amplifier

$$V_{out,1} = -V_1 \left( \frac{R_1}{R_2} \right)$$

$$V_{out,2} = V_2 \left( \frac{R_3}{R_3 + R_4} \right) \left( 1 + \frac{R_1}{R_2} \right)$$

$$V_{out} = \frac{R_1}{R_2} (V_2 - V_1)$$

$$\frac{R_2}{R_1} = \frac{R_3}{R_4}$$

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### Instrumentation Amplifier

$$V_{out} = \frac{R_1}{R_2} (V_{amp,b} - V_{amp,a})$$

$$I_x = \frac{V_1 - V_2}{R_x}$$

$$V_{amp,b} - V_{amp,a} = I_x (R_x + R_a + R_b)$$

$$V_{out} = \frac{R_1}{R_2} (V_2 - V_1) \left( 1 + \frac{R_a + R_b}{R_x} \right)$$

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### Loop-Gain Nyquist Criterion

$$A_{CL}(s) = G(s) \frac{A_{OL}(s)}{1 + \beta A_{OL}(s)}$$

- The system is unstable if the characteristic equation  $(1 + \beta A_{OL}(s))$  has roots in the right half of the complex plane
- Nyquist criterion is a test for location of  $(1 + \beta A_{OL}(s))$  roots
- Nyquist criterion can be viewed on the frequency domain (Bode)

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### Loop-gain on the frequency domain

In negative feedback systems  $\phi = 180^\circ (-180^\circ)$   
 At  $f \rightarrow 0$

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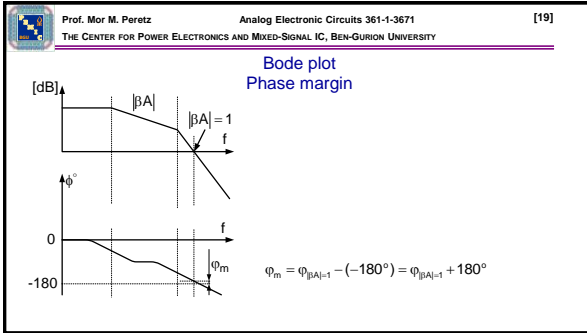
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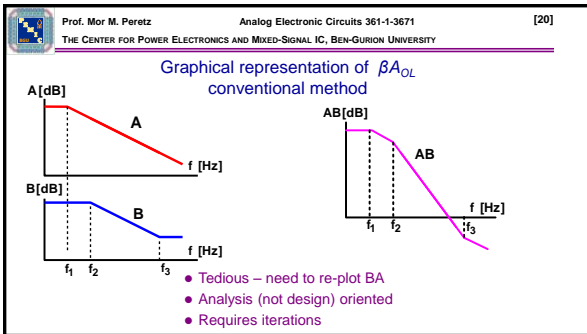
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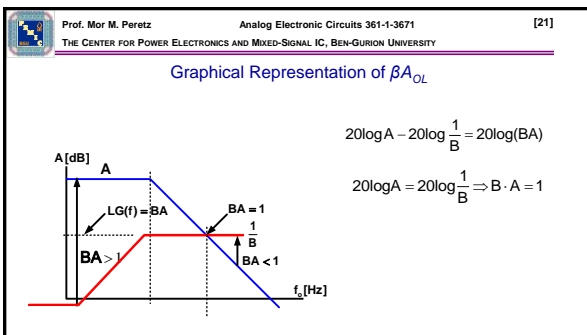
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### Possible compensations Rate of Closure (ROC)

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### Overshoot and Q in Closed Loop in Response to step in $S_{in}$

$Q \cong \frac{\sqrt{\cos\phi_m}}{\sin\phi_m}$  for  $\phi_m < 50^\circ$

**Design target  $\phi_m \geq 45^\circ$**

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