

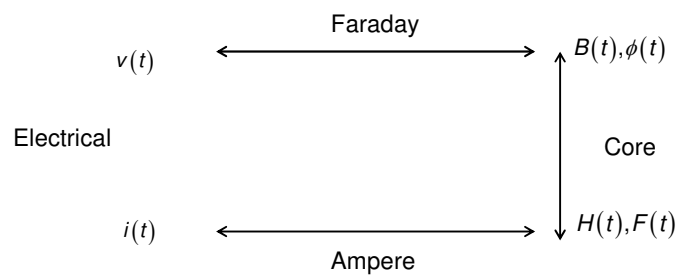


Magnetics

- Faraday's and Amper's laws
- Permeability
- Inductor
 - Reluctance model
 - Air gap
 - Current crowding
 - Inductor design
- Skin effect, proximity effect
- Losses
- Transformer
 - Ideal transformer
 - Real transformer
 - Transformer design

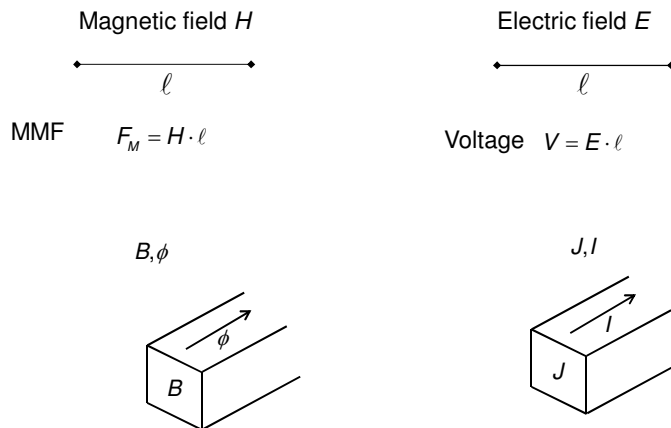


Important relationships

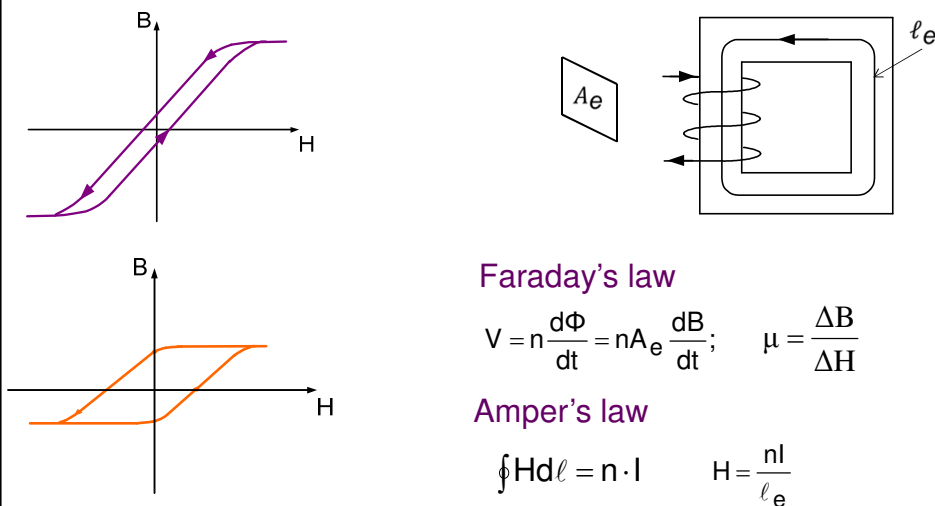




Magnetic quantities Analogies to electrical quantities



Important relationships





Units

Φ - magnetic flux Weber [Wb] V - voltage [V]

B - flux density $\frac{\text{Wb}}{\text{m}^2} = \text{Tesla [T]}$

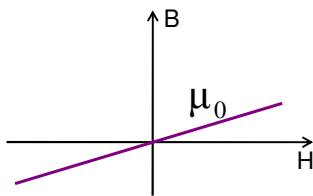
Gauss [G] 1T = 10,000 G

H - magnetic field [A/m]

μ - magnetic permeability [H/m]



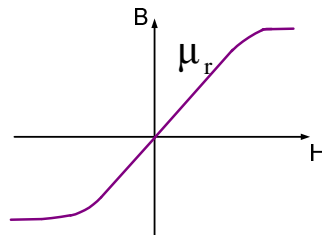
Permeability



Free space permeability
(Vacuum)

$$\mu_0 = 4\pi \cdot 10^{-7}$$

$$\mu = \frac{\Delta B}{\Delta H}$$



Typical B_{sat}

Ferrite: 0.2 – 0.5 T

Iron powder: 0.5 – 1 T

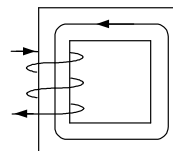
Typical magnetic material permeability

$$\mu_r = 10^3 - 10^5$$



What is inductance ?

$$V = n \frac{d\phi}{dt} \quad V = L \frac{di}{dt}$$



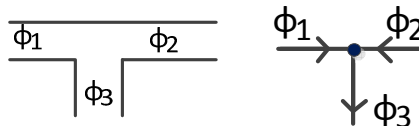
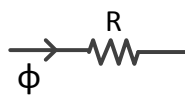
Reluctance model

$$F = Hl_e$$

$$H = \frac{B}{\mu} \quad B = \frac{\phi}{A}$$

$$R = \frac{l_e}{\mu A} \quad [H^{-1}]$$

$$F = \phi R$$



$$\phi_3 = \phi_1 + \phi_2$$



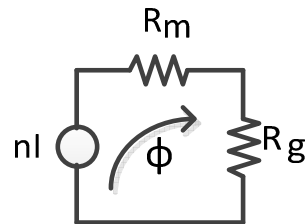
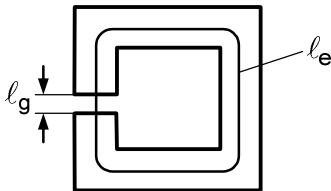
Inductance with gap

$$R_m = \frac{l_e}{\mu_r A_e}$$

$$R_g = \frac{l_g}{\mu_0 A_e}$$

$$nI = \phi (R_m + R_g)$$

$$v = n \frac{d\phi}{dt} = \underbrace{\frac{n^2}{R_m + R_g}}_L \frac{di}{dt}$$

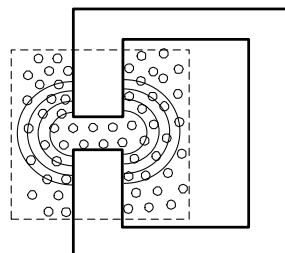
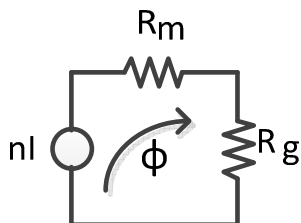


Current crowding

$$R_m = \frac{l_e}{\mu_r A_e}$$

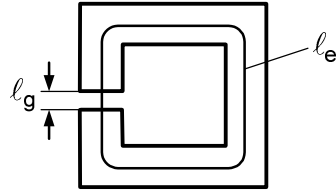
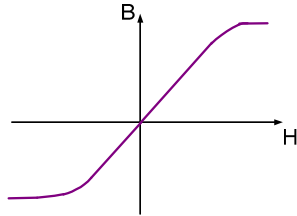
$$R_g = \frac{l_g}{\mu_0 A_e}$$

$$\frac{nI R_g}{(R_m + R_g)} \xrightarrow{R_g \gg R_m} nI$$





Inductor design Air gap



$$l_g \ll l_e$$
$$l_g + l_e \cong l_e$$

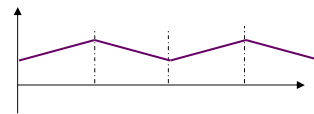
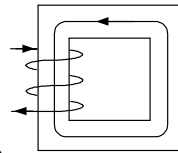
$$\text{If } \frac{l_e}{l_g} < \mu_r \quad \mu_{re} \approx \left(\frac{l_e}{l_g} \right)$$



Inductor design Saturation - Ae

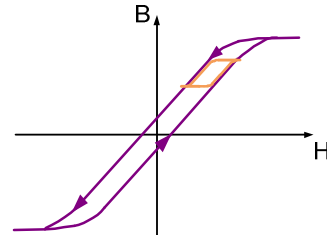
$$V = n \frac{d\Phi}{dt}$$

$$V = L \frac{di}{dt}$$



$$n A_e \int_0^{B_{max}} \left(\frac{dB}{dt} \right) dt = L \int_0^{i_{pk}} \left(\frac{di}{dt} \right) dt$$

$$L i_{pk} = n A_e B_{max}$$

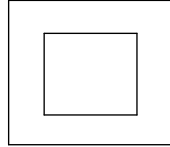


$$n = \frac{L i_{pk}}{B_{max} A_e}$$



Inductor design

A_w



$$A_w = \frac{nW_a}{k}$$

$$W_a = \frac{I_{rms}}{J}$$

$$A_w = \frac{nI_{rms}}{Jk}$$



Inductor design

A_p

$$A_p = A_e A_w = \frac{LI_{pk} I_{rms}}{B_{max} Jk}$$



Inductor design summary

- Calculate A_p
- Choose core
- Calculate n
- Calculate l_g or adjust gap



Inductor selection Off-shelf product



IHLP-1616BZ-11

Vishay Dale

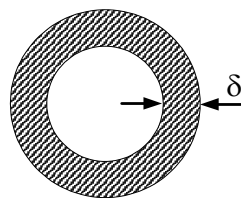
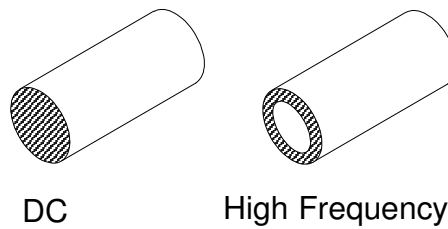
Low Profile,



Inductor selection Off-shelf product

STANDARD ELECTRICAL SPECIFICATIONS				
L_0 INDUCTANCE $\pm 20\%$ AT 100 kHz, 0.25 V, 0 A (μH)	DCR TYP. 25 °C (m Ω)	DCR MAX. 25 °C (m Ω)	HEAT RATING CURRENT DC TYP. (A) ⁽³⁾	SATURATION CURRENT DC TYP. (A) ⁽⁴⁾
0.10	4.1	4.5	12.0	12.0
0.22	6.5	7.0	9.0	9.0
0.47	14.5	16	7.0	7.0
1.0	24	27	4.5	5.0
2.2	61	68	3.25	3.25
4.7	95	105	1.7	1.75

Skin effect

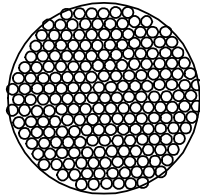


δ – skin depth

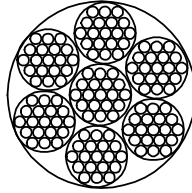
$$\frac{R_{AC}}{R_{DC}} > 1 \quad \delta \text{ (mm)} = \frac{72}{\sqrt{f}}$$

f in Hz

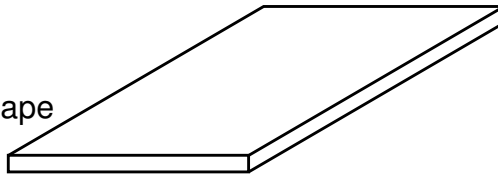
Skin Effect Solutions



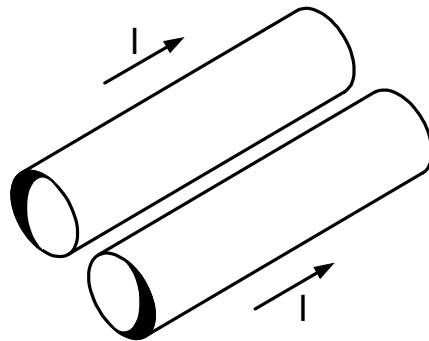
Litz wire



Foil/tape



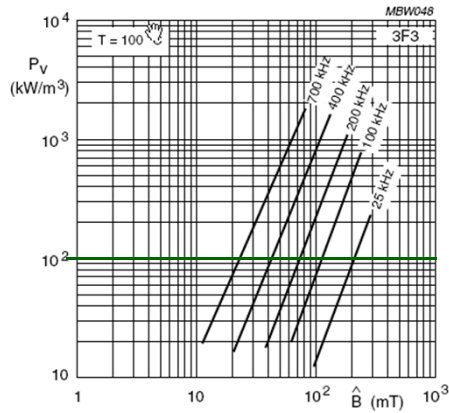
Proximity effect



Current crowding due to magnetic fields

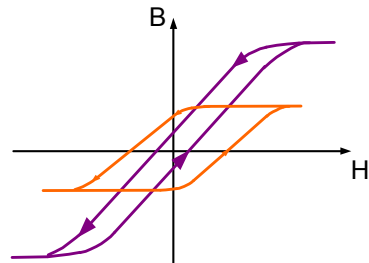


Losses function of ΔB

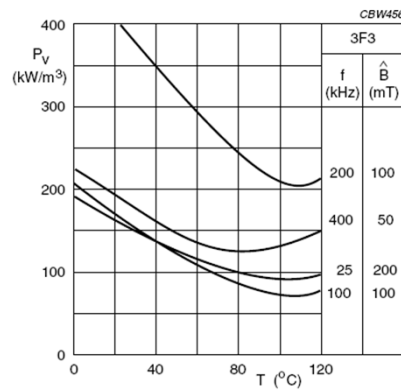


$$P \sim K \Delta B^i f^j$$

i, j – material dependent



Losses function of temperature





Losses material selection

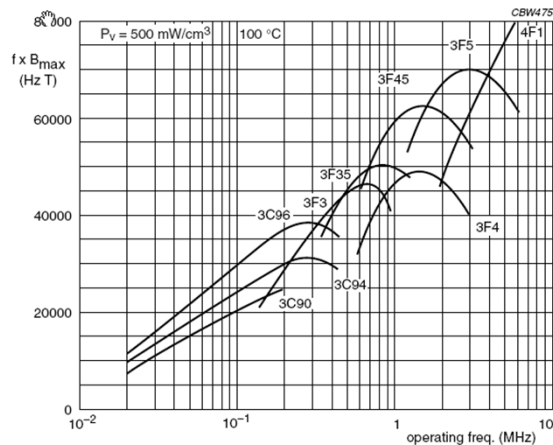
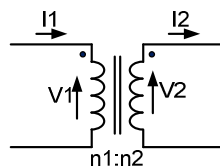


Fig.19 Performance factor ($f \times B_{max}$) at $PV = 500 \text{ mW/cm}^3$ as a function of frequency for power ferrite materials.



Ideal transformer

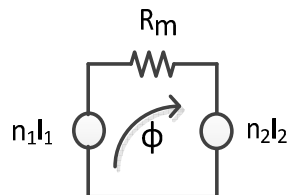
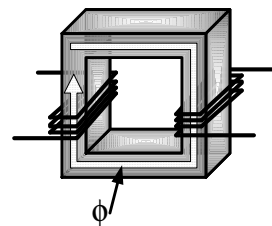


$$\phi R_m = n_1 I_1 - n_2 I_2$$

$$R_m \rightarrow 0$$

$$n_1 I_1 = n_2 I_2$$

$$V_1 = n_1 \frac{d\phi_1}{dt} \quad V_2 = n_2 \frac{d\phi_2}{dt}$$



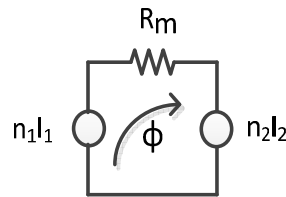
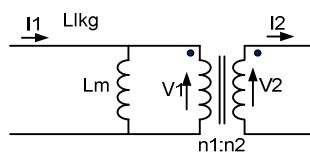


Transformer characteristics

- Current flow at the same time at primary and secondary
- Each winding represents inductance –
Average voltage = 0
- AC only on any winding



Magnetizing inductance



$$\phi R_m = n_1 I_1 - n_2 I_2$$

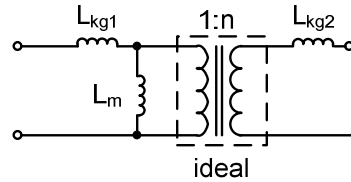
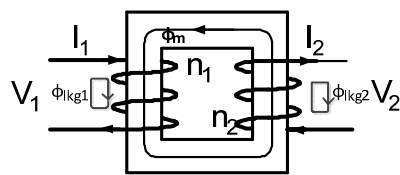
$$V_1 = n_1 \frac{d\phi}{dt}$$

$$V_1 = \underbrace{\frac{n_1^2}{R_m}}_{L_m} \frac{d}{dt} \left(i_1 + i_2 \frac{n_2}{n_1} \right)$$



Leakage inductance

- uncoupled magnetic flux



L_{lkg} , M (mutual coupling) and k (coupling coefficient)

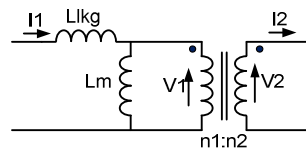
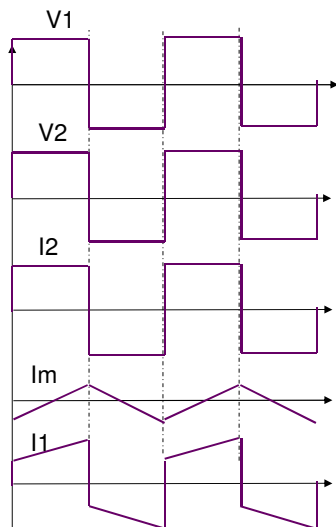
$$M = k\sqrt{L_1 \cdot L_2}$$

$$L_{lkg1} \cong L_m(1 - k)$$

$$L_{lkg2} \cong L_{lkg1} \cdot n^2$$



Magnetizing and leakage inductances





Transformer design

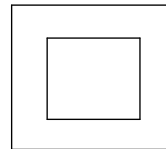
A_w

$$A_w = \frac{n_1 W_{a1} + n_2 W_{a2}}{k}$$

$$W_a = \frac{I_{rms}}{J}$$

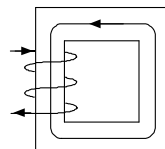
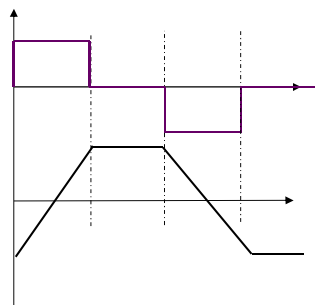
$$A_w = \frac{n_1 I_{1rms} + n_2 I_{2rms}}{Jk}$$

$$A_w = \frac{2n_1 I_{1rms}}{Jk}$$



Transformer design

Saturation - A_e



$$B = \frac{1}{nA_e} \int V dt$$

$$|B_{max}^+| = |B_{max}^-|$$

$$n = \frac{V_m T_{on}}{2 B_{max} A_e}$$



Transformer design

A_p

$$A_p = A_w A_e = \frac{\{V_1 \cdot T_{on}\} 2 \cdot I_{1rms}}{\{2B_{max}\} Jk}$$

$$A_p = \frac{\{V_1 \cdot T_{on}\} 2 \cdot I_{1rms}}{\Delta B \cdot Jk}$$

$$A_p = \frac{\{V_1 \cdot D_{on}\} 2 \cdot I_{1rms}}{f_s \cdot \Delta B \cdot Jk}$$



Transformer design summary

- Calculate A_p
- Choose core
- Calculate n_1
- Calculate n_2



Magnetic design Example

- Boost converter: $P=100\text{W}$, $V_{in}=10\text{V}$, $V_o=50\text{V}$, $\Delta I_L=0.1I_{L_{av}}$
- Calculate L
- Calculate A_p





