

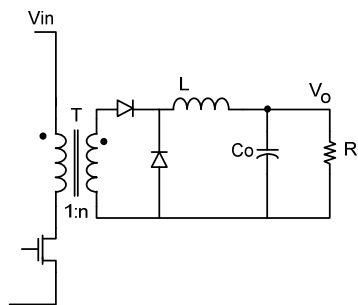
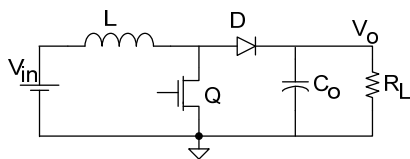


## Drivers

- What is a driver
- MOSFET capacitances
- Driver operation
- Gate capacitance
- Gate drive calculation
- Driver types
  - High-side driver
    - Isolation
    - Optocoupler
    - Boot-strap supply

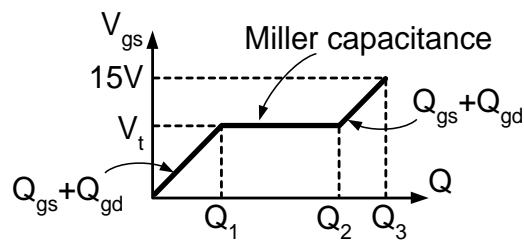
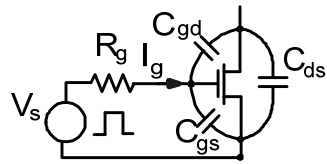


## Driver

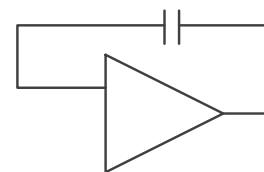
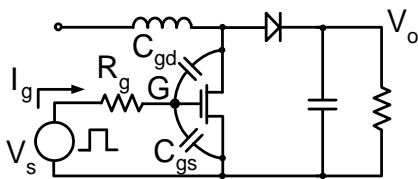




### MOSFET capacitances



### Miller effect



$$V_{Cgs}(0) = 0 \quad V_{Cgs}(\infty) = V_{GSmax}$$

$$V_{Cgd}(0) = -V_O \quad V_{Cgd}(\infty) = V_{GSmax}$$

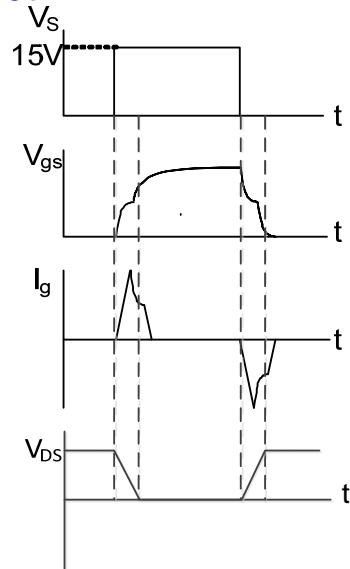
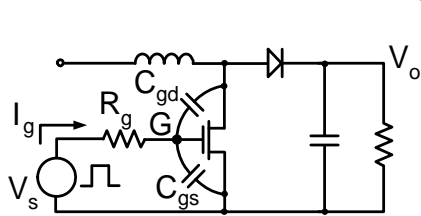
$$C_m = C[1 - (-k)] = C[1 + k]$$

$$Q_{total} = V_{GS} C_{gs} + (V_{GS} + V_O) C_{gd}$$

$$C_{eq} = \frac{Q_{total}}{V_{GSmax}} = C_{gs} + C_{gd} \left(1 + \frac{V_o}{V_{GSmax}}\right)$$

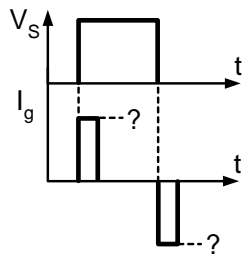


### Miller effect



### Required drive calculation Equivalent capacitance

Assuming constant drive current



$$C_{eq} = C_{gs} + C_{gd} \left(1 + \frac{V_o}{V_{GS\max}}\right)$$

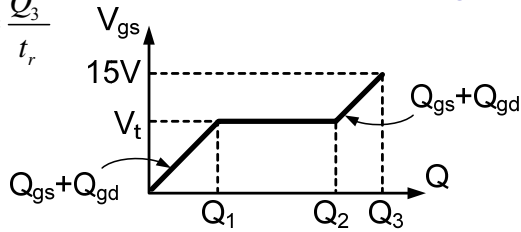
$$Q_{total} = I_g \cdot t_{on} = C_{eq} \cdot V_{gs\max}$$

$$I_g = \frac{C_{eq} V_{gs\max}}{t_{on}}$$

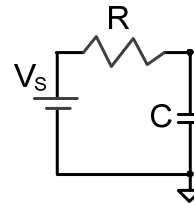


### Required drive calculation Gate charge

$$I_g = \frac{Q_3}{t_r}$$



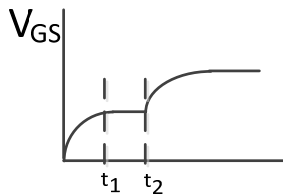
For  $t_1$



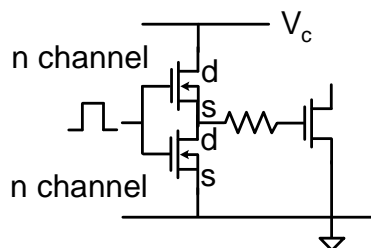
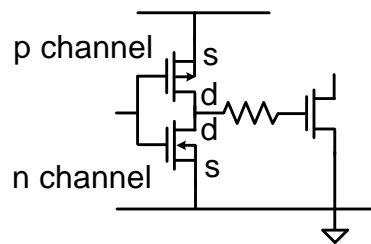
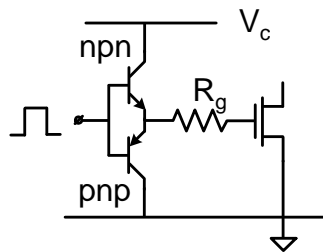
For  $t_2$

$$\Delta Q = \Delta I \cdot t_2$$

$$\Delta I = \frac{\Delta V}{R_g}$$

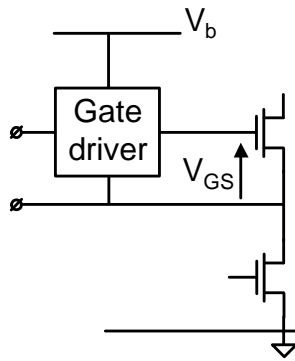


### Driver types

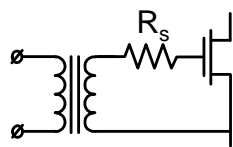




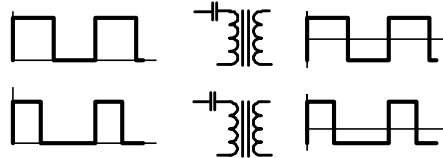
## High-side driver



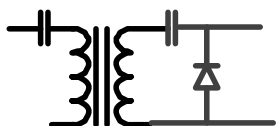
## High-side driver Transformer



Problem of large Don

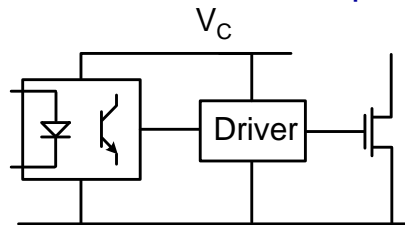


Possible solution: DC restorer





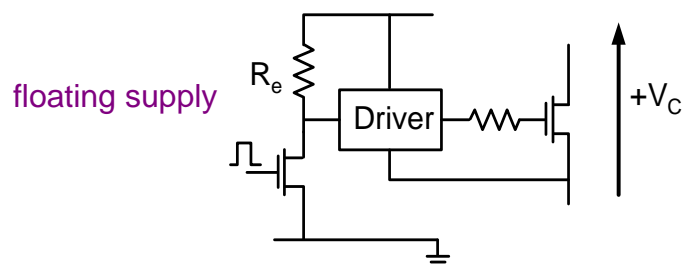
## High-side driver Optocoupler



$V_C$  - floating supply



## High-side driver Potential offset

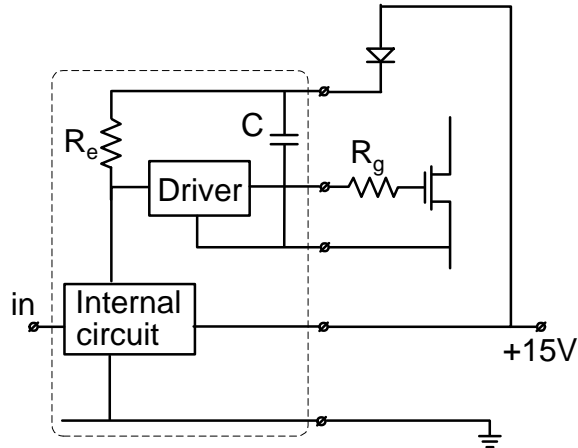


floating supply

Logic signal is referred to GND  
FET is used to sustain the high voltage



## High-side driver Boot-strap supply – floating capacitor



## High-side driver Boot-strap supply – commercial product

buffer stage designed for minimum driver production. Propagation delays are matched for use in high frequency applications. The channel can be used to drive an N-channel MOSFET or IGBT in the high side configuration up to 500 or 600 volts.

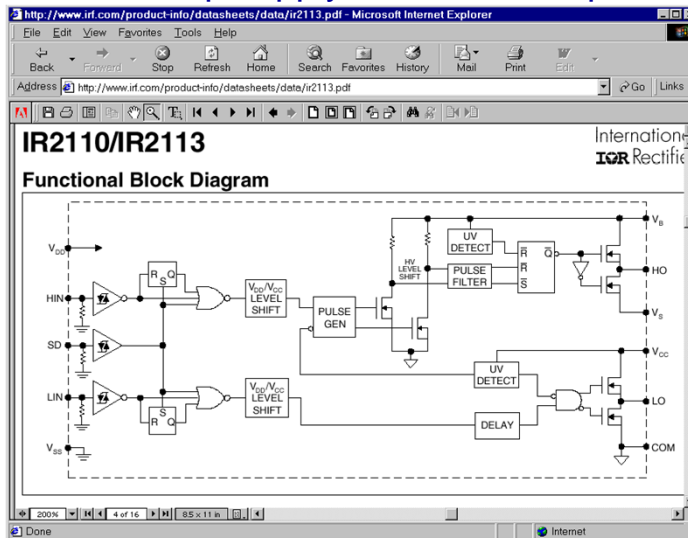
**Physical Connection**

up to 500V or 600V

TO LOAD



## High-side driver Boot-strap supply – commercial product

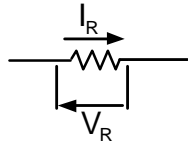


## Current sensing

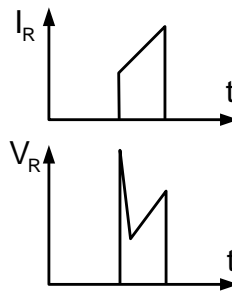
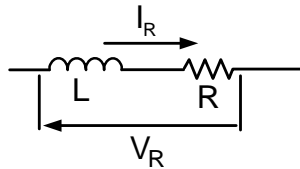
- Resistive sensing
- Current transformer
- Measuring DC
- Reset
- Design
- Hall effect



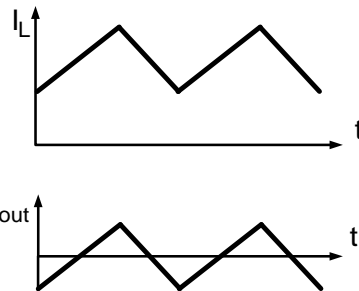
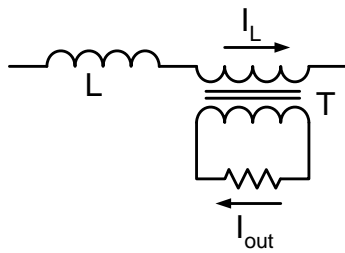
## Resistive sensing



Parasitic inductance



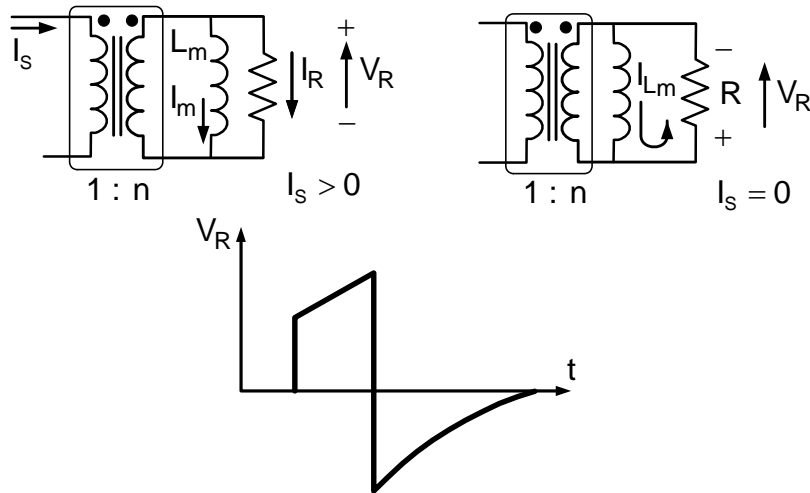
## Current transformer



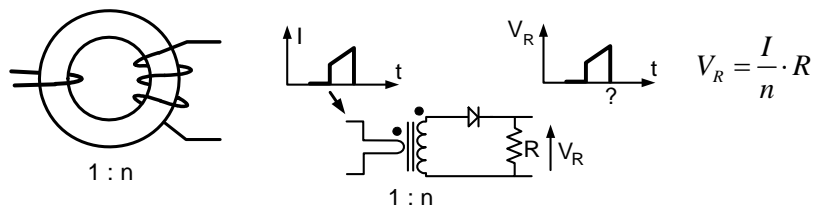
DC component via primary lost  
DC component may saturate transformer



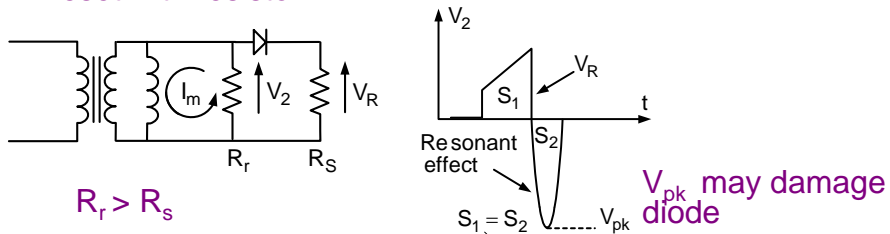
### Current transformer Pulse current - Problem due to reset



### Pulse current transformer

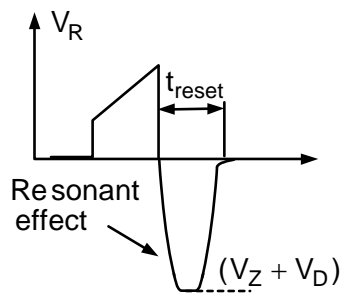
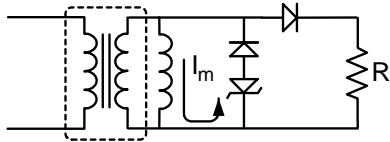


#### Reset with resistor

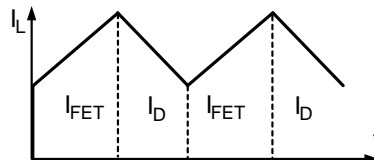
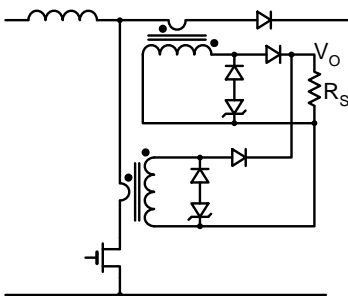




## Pulse current transformer Reset with clamp

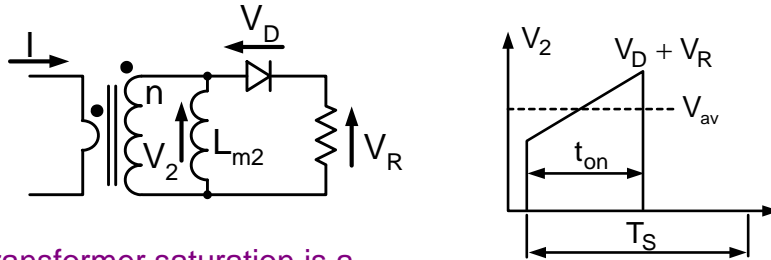


## Measuring inductor current Combining two sensors





### Design of current transformer



Transformer saturation is a function of the **voltage**

$$B_{max} = \frac{\int Vdt}{nA_e} \quad V_R \cong \frac{I}{n} R$$

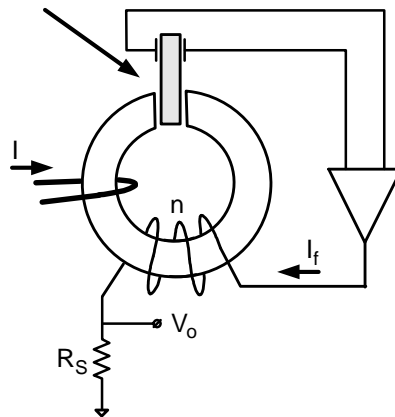
$$B_{max} = \frac{I_{av} R D_{max}}{nA_e f_s}$$

$$\int Vdt = V_{av} t_{on} = \frac{V_{av} D_{on}}{f_s}$$




### Hall Effect sensor

Active Device  
Hall effect sensor

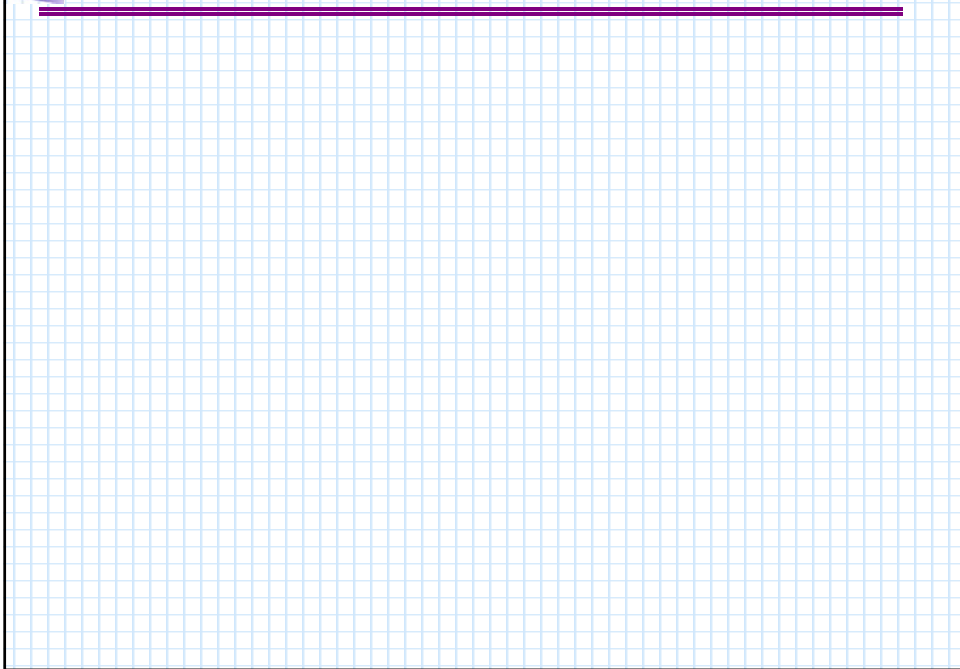



Zeroing the flux by feedback

$$I_f \cdot n = I \quad V_o = \frac{I}{n} R_s$$

 **Mor M. Peretz, Switch-Mode Power Supplies** **[7-25]**

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 **Mor M. Peretz, Switch-Mode Power Supplies** **[7-26]**

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